



## Incorporation of fillers in elastomeric composites: impact of the process on the thermomechanical properties

Adrien Simon, Daphné Berthier, Marie-Pierre Deffarges, Mathieu Venin,  
Florian Lacroix, Yoann Tendron, Stéphane Méo

### ► To cite this version:

Adrien Simon, Daphné Berthier, Marie-Pierre Deffarges, Mathieu Venin, Florian Lacroix, et al.. Incorporation of fillers in elastomeric composites: impact of the process on the thermomechanical properties. IRC 2019, Sep 2019, London, United Kingdom. hal-02294357

HAL Id: hal-02294357

<https://univ-tours.hal.science/hal-02294357>

Submitted on 23 Sep 2019

**HAL** is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

# Incorporation of fillers in elastomeric composites: impact of the process on the thermomechanical properties

Adrien Simon, Daphné Berthier<sup>2</sup>, Marie-Pierre Deffarges<sup>1</sup>, Mathieu Venin<sup>1</sup>, Florian Lacroix<sup>1</sup>, Yohan Tendron<sup>2</sup>, Stéphane Méo<sup>1</sup>

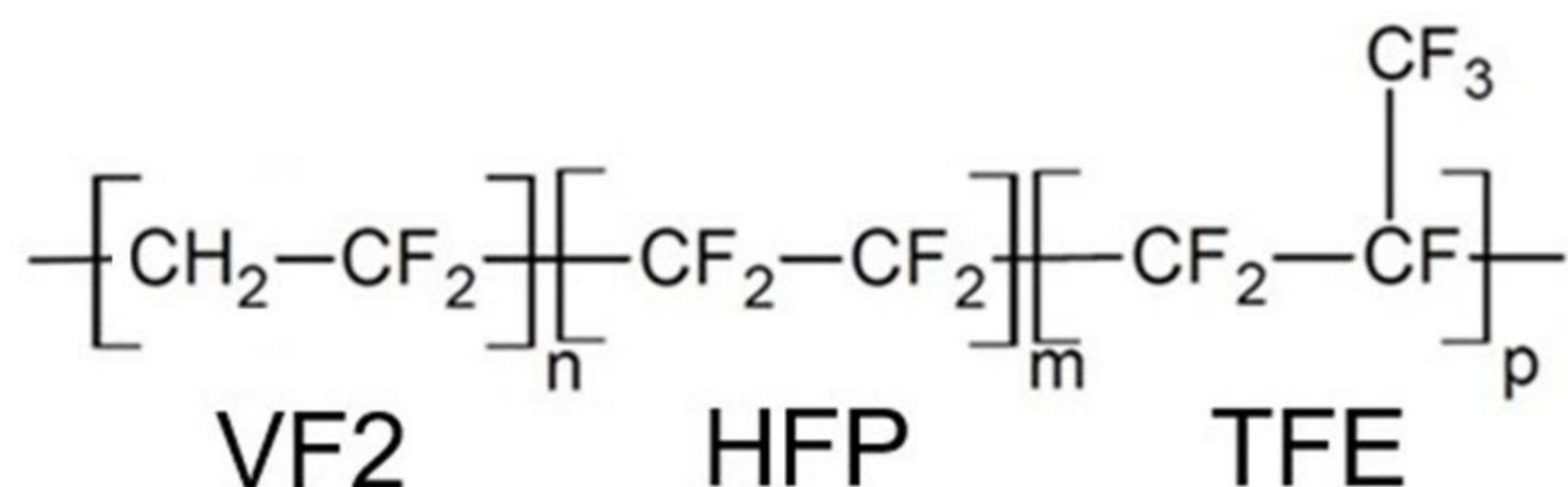
<sup>1</sup> Laboratoire de Mécanique Gabriel Lamé, Université de Tours, Université d'Orléans, INSA Centre Val de Loire, Polytech Tours, 7 avenue Marcel Dassault BP40, 37004 Tours, France

<sup>2</sup> SAFRAN AEROSYSTEMS, 20 Avenue Georges Pompidou, 37600 Loches, France

\* In partnership with the LRCCP (Laboratoire de Recherche et de Contrôle du Caoutchouc et des Plastiques)

Previous works [1] led to the development of a new formula on the basis of FKM blend reinforced with Polyhedral Oligomeric Silsesquioxanes (POSS). The main objective consists in maintaining thermomechanical properties while changing the process scale. To this end, two new specimen geometries of vulcanized rubber are studied : thin films obtained by coating at laboratory scale through masterbatch and sheets obtained through rubber mill and thermocompression.

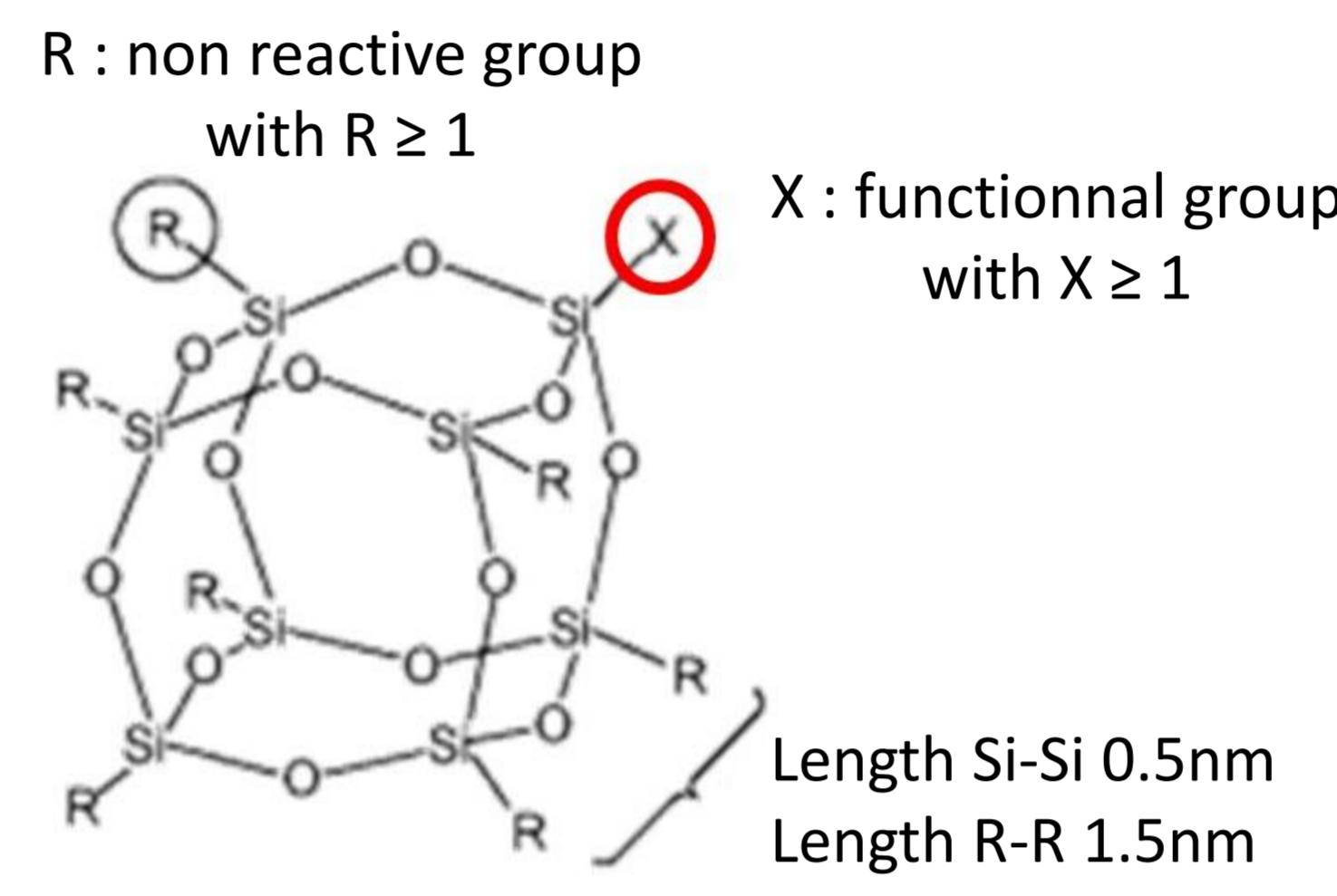
## Fluorinated rubber: FKM



Formula of the terpolymer FKM

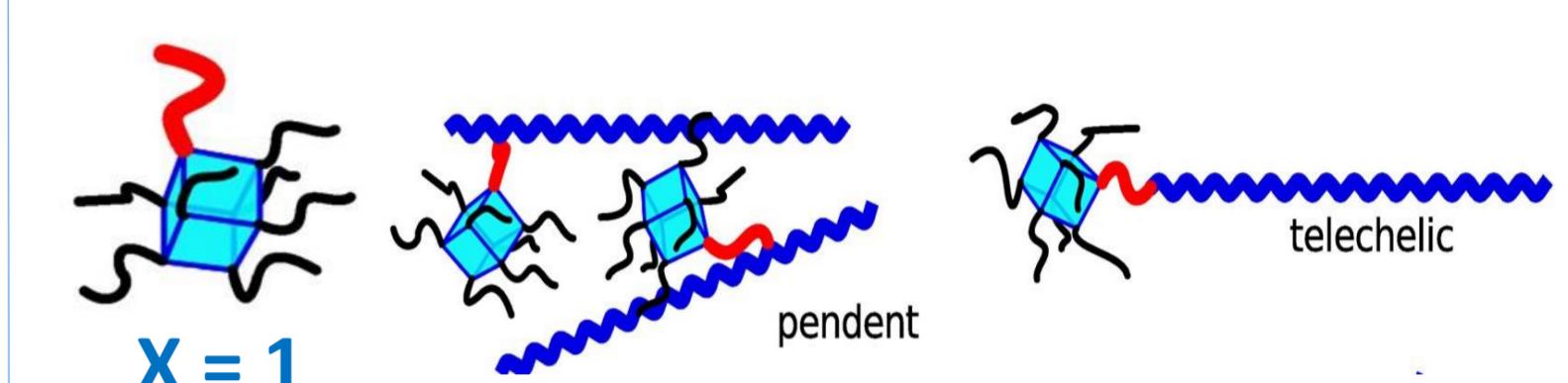
- A fourth monomer is incorporated to enhance the crosslinking action, named « Cure Site Monomer » (CSM)
- FKM exhibits good mechanical, chemical and thermal properties

## Polyhedral Oligomeric Silsesquioxanes (POSS)



Chemical structure of POSS

- Smallest silica particles (1 to 3nm)
- Hybrid chemical composition
- Role of functional groups (X) : chemical interaction with polymers



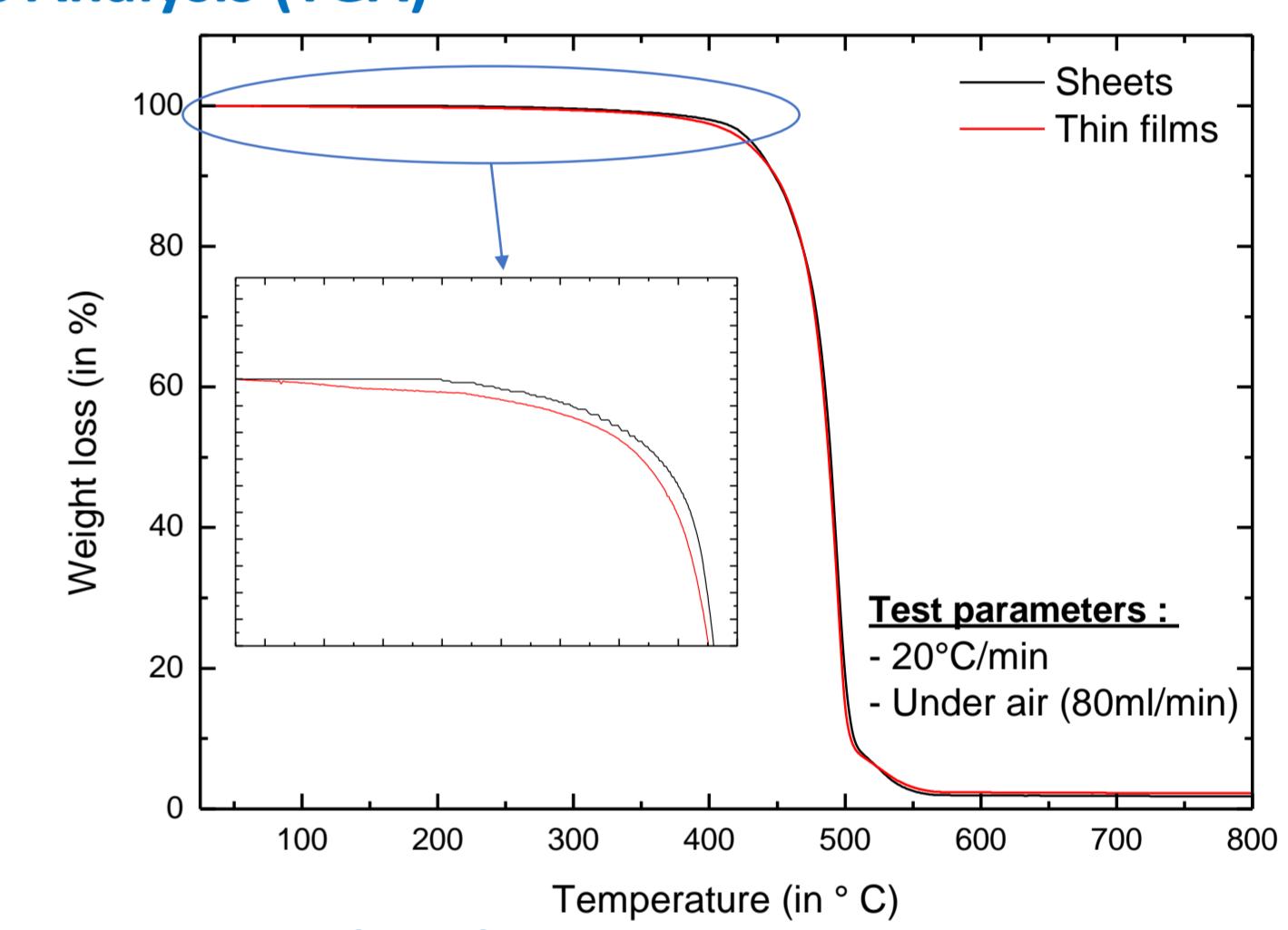
Possible interactions with a POSS (X=1) [2]

## Two studied processes Main parameters

	Coating	Thermocompression
1. Mixing step	<p>Dispersion in solvent</p> <ul style="list-style-type: none"> <li>▪ Order of incorporation</li> <li>▪ Solvent, temperature, stirring rate</li> </ul> <p>Deposition rate</p>	<p>Rubber mill</p> <ul style="list-style-type: none"> <li>▪ Order of incorporation</li> <li>▪ Rotation speed</li> <li>▪ Temperature</li> </ul>
2. Vulcanising process (Vulcanization + Post-vulcanization)	<ul style="list-style-type: none"> <li>▪ Cycles (Temperature, time)</li> <li>▪ Specimen volume ≈ 0,4 cm<sup>3</sup></li> </ul>	<ul style="list-style-type: none"> <li>▪ Cycles (Temperature, time, pressure)</li> <li>▪ Specimen volume ≈ 40 cm<sup>3</sup></li> </ul>
3. Specimen geometries	<ul style="list-style-type: none"> <li>▪ Dimension: Thickness : around 400 µm</li> </ul>	<ul style="list-style-type: none"> <li>▪ Dimension: Thickness : around 2 mm</li> </ul>

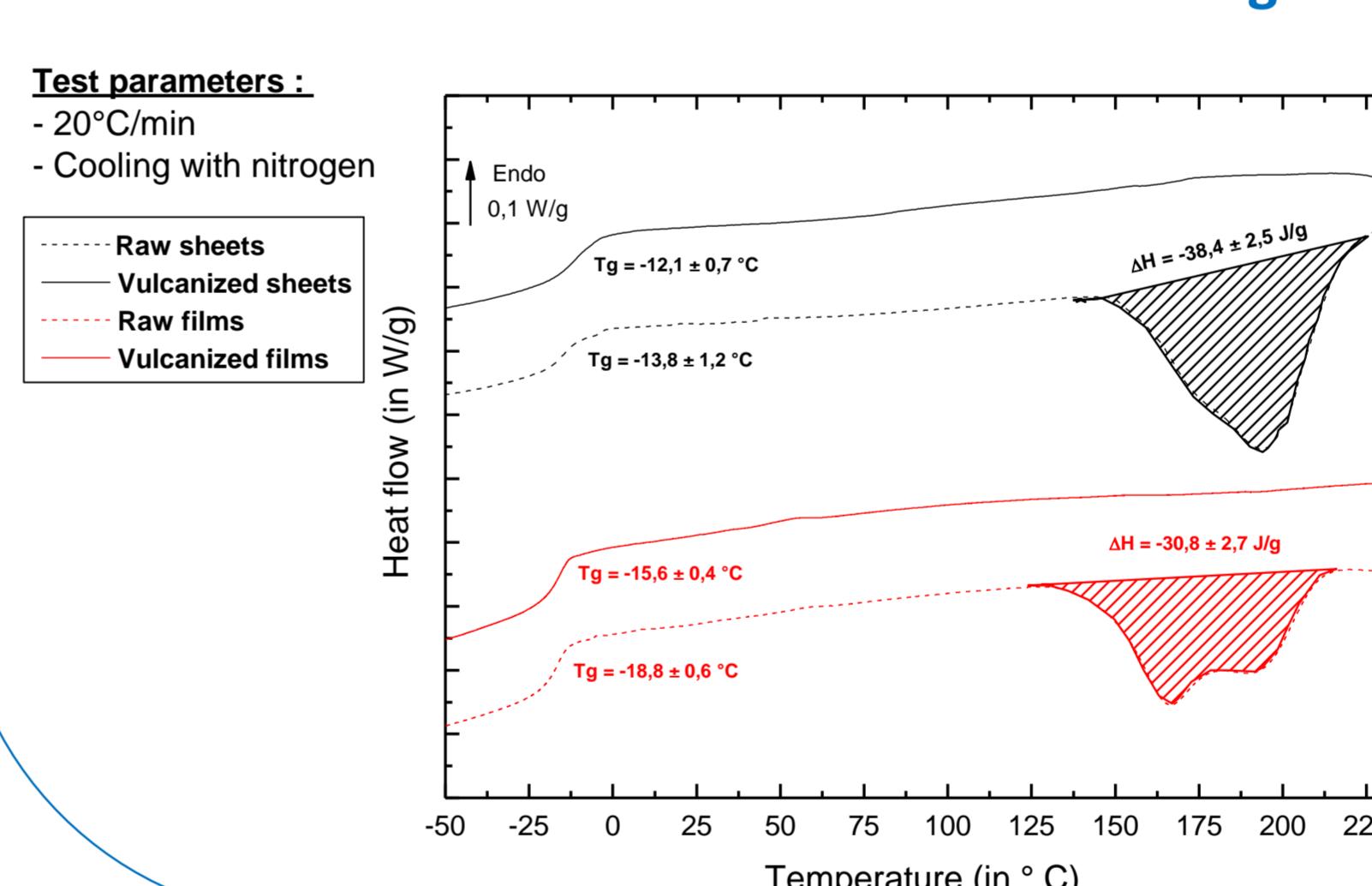
## Thermal behaviour

### ThermoGravimetric Analysis (TGA)



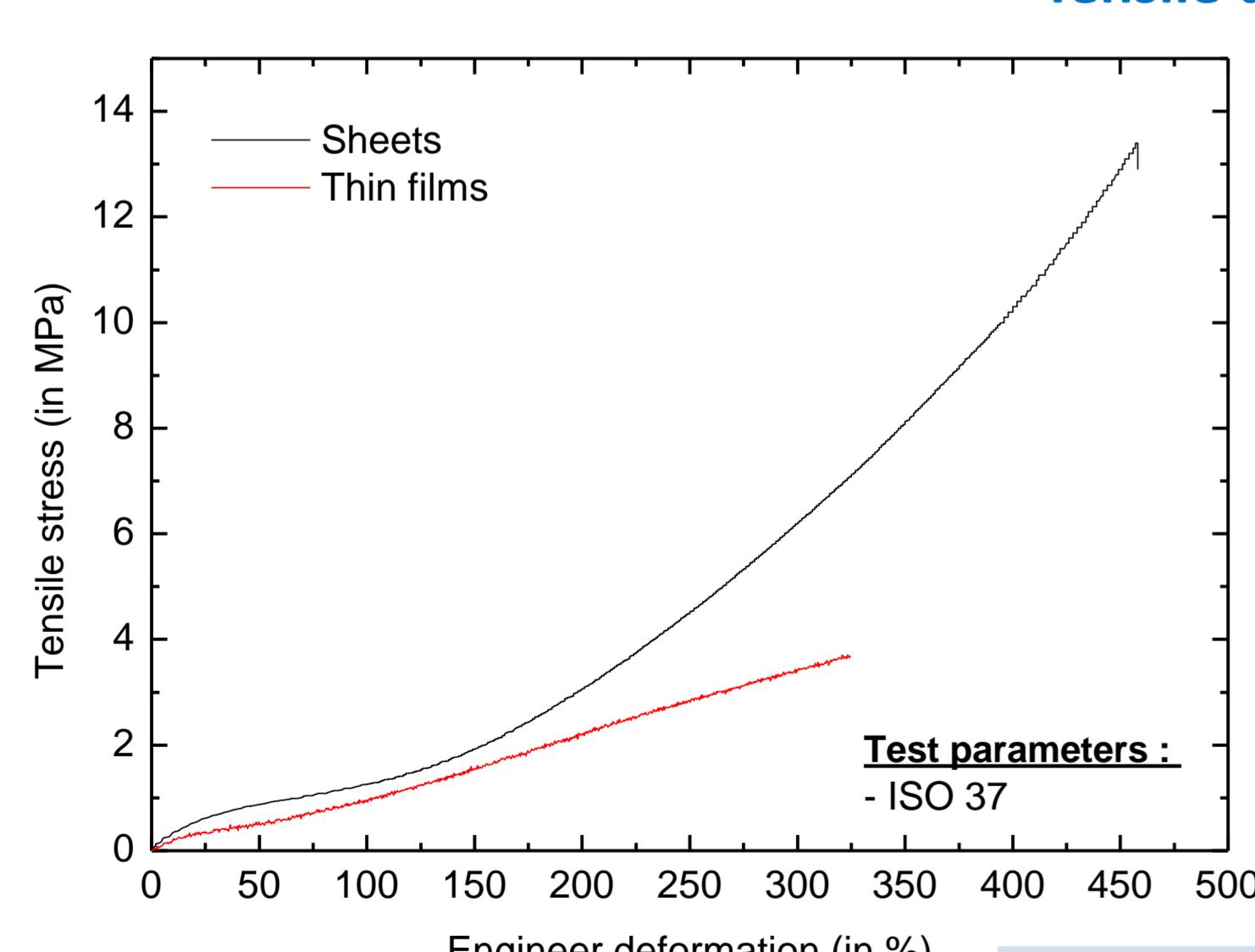
$$T_{\text{degradation at 50 \%}} = 488 \text{ }^{\circ}\text{C}$$

### Differential Scanning Calorimetry (DSC)



- The glass transition (for raw and vulcanized samples), the activation temperature and the reaction area of the crosslinking reaction are higher by thermocompression than by coating

## Tensile tests at 23°C

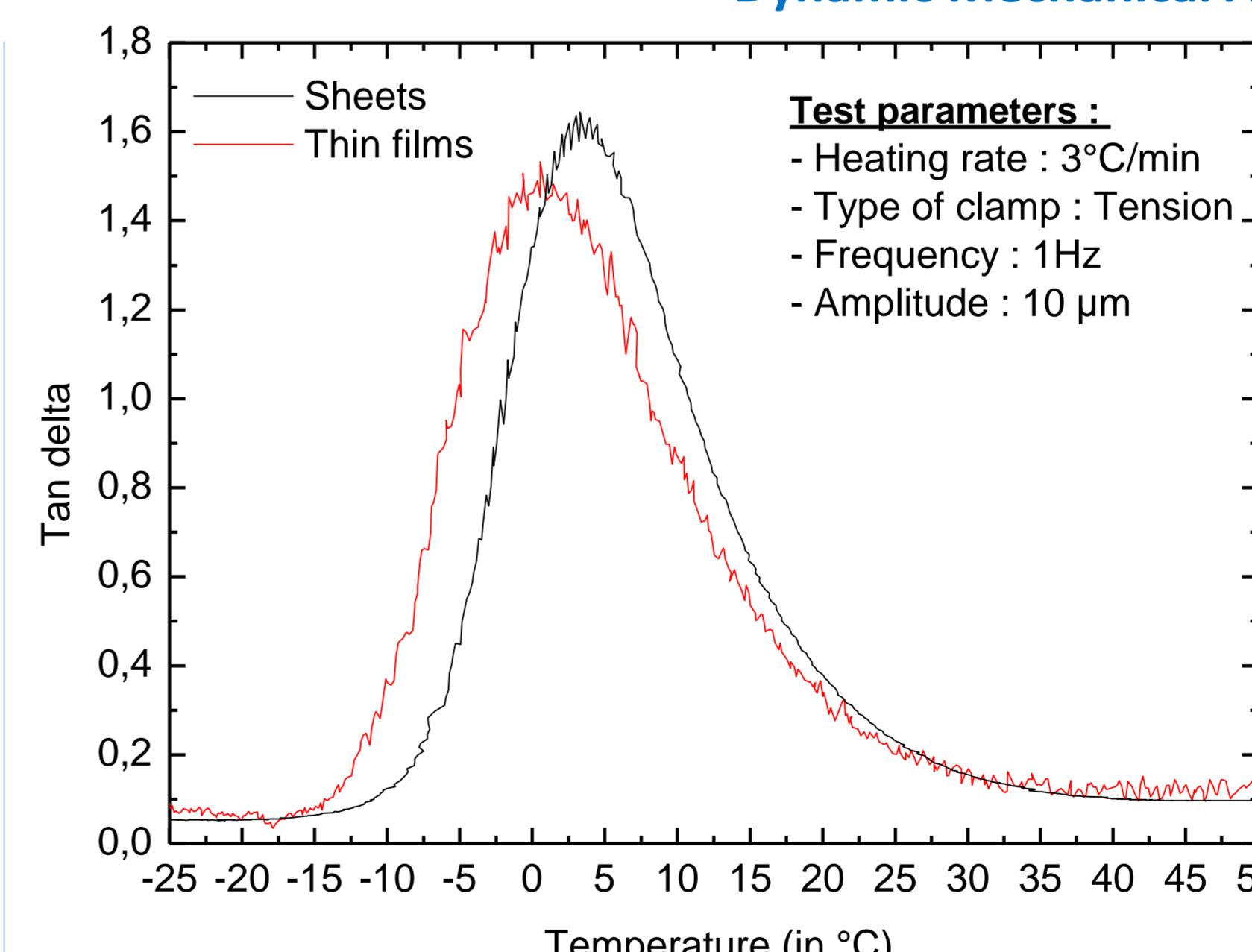


- Curve trends and failure parameters are different between thin films and sheets

	Modulus at 100% (in MPa)	Tensile at failure (in MPa)	Elongation at failure (in %)
Thin films	0.6 ± 0.05	2.4 ± 0.7	278 ± 45
Sheets	1.24 ± 0.01	11.2 ± 1.5	425 ± 30

## Mechanical behaviour

### Dynamic Mechanical Analysis (DMA)



$$\text{T}_\alpha \text{ (in } ^\circ\text{C) at 1 Hz}$$

Thin films	1.4 ± 0.2
Sheets	2.7 ± 0.6

$$\text{T}_\alpha \text{ Sheet} > \text{T}_\alpha \text{ Thin film}$$

## Conclusions

- Impact of the process and of the specimen geometries on the macroscopic mechanical characterisation (by tensile test : underestimation of the materials properties on thin films), on the glass transition and on the cross linking reaction (on activation energy and activation temperature)
- Presence of volatile compounds in thin films but not in sheets (TGA results)
- No impact on degradation behaviour
- Thin films is a cost efficient way to provide thermal informations before sheet fabrication

## Perspectives

### Processes and geometries

- Impact of a new manufacturing way (tube by extrusion)
- Comparison between the three final products (thin film-sheet-tube)

### Upgrade of the formula

- Incorporation of POSS with new functional groups
- Characterisation of materials after chemical and/or thermal aging